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# Signal propagation parameters estimation through designed multi layer fibre with higher dominant modes using OptiFibre simulation

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**Abstract:** The aim and scope of the paper is to simulate the signal propagation parameters estimation through designed multi-layer fibre with higher dominant modes by using OptiFibre simulation software. The multi-layer fibre profile has a length of 1000 m is designed and clarified with six layers. RI difference profile variations are clarified with radial distance variations. Modal/group index, group delay, dispersion, mode field diameter and total fibre losses are demonstrated with the fibre wavelength variations. All the dominant mode field distribution for multi-layer fibre are simulated and demonstrated. The other modes for designed multi-layer fibre with the theoretical fibre cutoff values for the different modes based the designed multi-layer fibre are analyzed and clarified clearly in details.

**Keywords:** dominant modes; multi layer fibre; parameters estimation; signal propagation.

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## 1 Introduction

Imperfection losses include bending, coupling and splicing losses [1–9]. They arise because of stress from the manufacturing, environment and physical bending. Joint or splicing losses arise from inherent problems of connection when jointing fibres like different diameters of core and/or cladding, different relative index differences and/or numerical aperture, different RI profiles and fibre faults [10–18]. The configurations of optical fibres can be further categorized according to both of the index profile of fibre and the modes propagating through it into three types. The SMF-SI fibre has a central core which is significantly small such that there is only one light path for propagation within fibre. The core diameter of SMF-SI fibre is smaller (8–12  $\mu\text{m}$ ) than that of MMFs. In the SMF-SI, all light rays arrive at the same time to the end. Manufacturing and handling of SMF-SI fibre is so difficult [12]. The MMF-SI fibre is the simplest type. It includes glass, PCS and plastic fibres. Its fabrication is easy. It has a core diameter (50–1000  $\mu\text{m}$ ) [19–28].

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This leads to large aperture enabling more light to enter the fibre. Light rays travel in a zigzag path. There are many pathways that light ray takes during propagation [29–36]. MMF-SI fibre has profile index that takes steps from low to high and from high to low when measuring from cladding to core to cladding. The drawback of MMF-SI fibre is the different lengths of optical paths caused by various angles of light propagation [37–44].

The good results can be achieved with the same or compatible fibres. But there are still some jointing problems like mechanical alignment between two fibres being to be jointed, the quality of end-face of fibre and cleanliness of end-faces of fibre. The possible misalignment may result in three dimensions which are [45–54]: the longitudinal misalignment (the separation between fibres). The effective acceptance angle of the graded index (GI) fibre is slightly less than step index (SI) fibre. This makes coupling fibre to the light source more difficult. GI fibre has a higher bandwidth and a lower coupling efficiency than the SI fibre [55–61]. It is commercially available in sizes of 50/125 and 62.5/125. The 50/125 fibre with a smaller NA and higher bandwidth is improved for long haul communications [62–78]. The 62.5/125 fibre is enhanced for LAN networks [79–98].

## 2 Multi-layer fibre profile description

Figure 1 demonstrates the multi-layer fibre profile description. The fibre construction composed of six layers. Region 0 (first fibre layer) has a constant refractive index (RI) profile of 1.45 with 10 µm width. Region 1 (second fibre layer) has a parabolic fibre profile with the starting RI of 1.445 and

ending RI of 1.4456 with 10 µm width. Region 2 (third fibre layer) has exponential RI profile with the starting RI of 1.445 and ending RI of 1.45 with width of 20 µm. The fibre wavelength varies from 0.85 to 1.65 µm. The designed multilayer fibre has 1000 m length of and 20 m coupling length.

Region 3 (fourth fibre layer) has a Gaussian fibre profile with max RI of 1.445, normalized full width half max (FWHM) value of 10 with 30 µm width. Region 4 (fifth fibre layer) has alpha peak fibre profile with max RI of 1.445, normalized index difference (NID) value of 0.4 and alpha value of 2 with 10 µm width. Region 5 (sixth fibre layer) has alpha dip fibre profile with max RI of 1.445, NID value of 0.4 and alpha value of 2 with 10 µm width. The designed multi-layer fibre model description is clarified against radial distance ( $x$ ) in Figure 1. The six fibre layers are composed of the alpha-dip, linear, parabolic, exponential, Gaussian and alpha-peak fibre profiles which are estimated by [10, 11, 19–22]:

$$n(x) = n_{\max} \exp \left[ -\ln 2 \left( \frac{2(x-x_0)}{h.w} \right)^2 \right] \text{ [Gaussian Profile]} \quad (1)$$

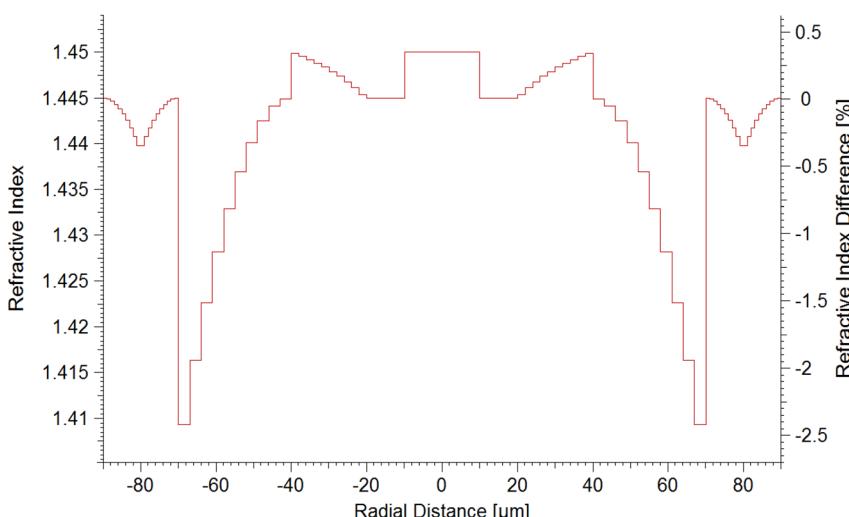
$$n(x) = n_{\max} \sqrt{1 - 2\Delta \left( \frac{x}{w} \right)^{\alpha}} \text{ [Alpha Peak Profile]} \quad (2)$$

$$n(x) = n_{\max} \sqrt{1 - 2\Delta \left( 1 - \frac{x}{w} \right)^{\alpha}} \text{ [Alpha dip Profile]} \quad (3)$$

$$n(x) = n(0) + x \cdot \frac{n(w) - n(0)}{w} \text{ [Linear Profile]} \quad (4)$$

$$n(x) = [n(w) - n(0)] \cdot \left( \frac{x}{w} \right)^2 + n(0) \text{ [Parabolic Profile]} \quad (5)$$

$$n(x) = [n(w) - n(0)] \cdot \frac{e}{e-1} \exp \left( -\frac{x}{w} \right) + \frac{e \cdot n(w) - n(0)}{e-1} \text{ [Exponential Profile]} \quad (6)$$



**Figure 1:** Designed multi-layer fibre model description.

with  $x$  is the radial distance,  $w$  is the layer width,  $n_{\max}$  is the max value,  $x_0$  is the position and  $\Delta$  is the difference is represented by the following formula [10, 11, 19]:

$$\Delta = \frac{n_{\max}^2 - n_{\min}^2}{2n_{\max}^2} \quad (7)$$

The group delay, total dispersion and the effective mode field diameter can be represented by the following formulas [7, 19–22]:

$$T_g = -\frac{2\pi c z}{\omega^2} \left( k_0 \frac{dn}{d\lambda} + n \frac{dk_0}{d\lambda} \right) = \frac{z}{c} \left( n - \lambda \frac{dn}{d\lambda} \right) \quad (8)$$

$$D_{\text{total}} = -\frac{z\lambda}{c} \left( \frac{d^2 N_{\text{eff}}}{d\lambda^2} \right) \quad (9)$$

$$d_{\text{eff}} = \frac{2}{\sqrt{\pi}} \sqrt{A_{\text{eff}}} \quad (10)$$

with the wave number  $k_0 = 2\pi/\lambda$ ,  $A_{\text{eff}}$  is the effective area. Where the macro and micro-fibre losses are estimated by [6, 19–21]:

$$\alpha_{\text{macro}} = \frac{10}{z} \log(\exp[yz]) \quad (11)$$

$$\alpha_{\text{micro}} = A (kn_1 d_n)^2 (kn_1 d_n^2)^{2p} \quad (12)$$

with  $A$  is a constant,  $p$  is the exponent power law. The splice losses can be given by [6, 7, 10, 11, 19–22]:

$$\alpha_{\text{Splice}} = -10 \log \left[ \left( \frac{16 n_1^2 n_2^2}{(n_1 + n_2)^4} \right) \sigma \exp \left( \frac{-\rho u}{q} \right) \right] \quad (13)$$

where the parameters  $\rho$ ,  $q$  are calculated by the following formulas [7, 10, 19–21]:

$$\rho = \frac{(k w_1^2)}{2} \quad (14)$$

$$q = G^2 + \frac{(\sigma + 1)^2}{4} \quad (15)$$

with the parameters  $\sigma$  and  $G$  are estimated by [6, 7, 11, 19–21]:

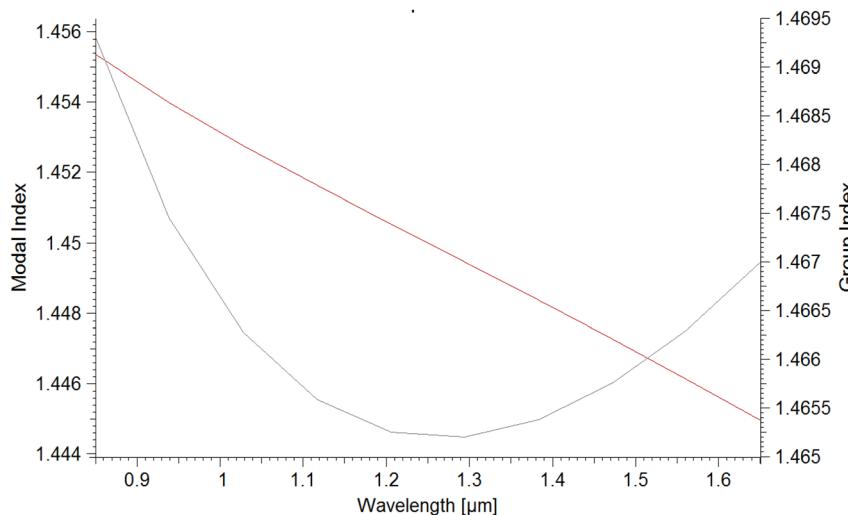
$$\sigma = \left( \frac{w_2}{w_1} \right)^2 \quad (16)$$

$$G = \frac{z}{k w_1^2} \quad (17)$$

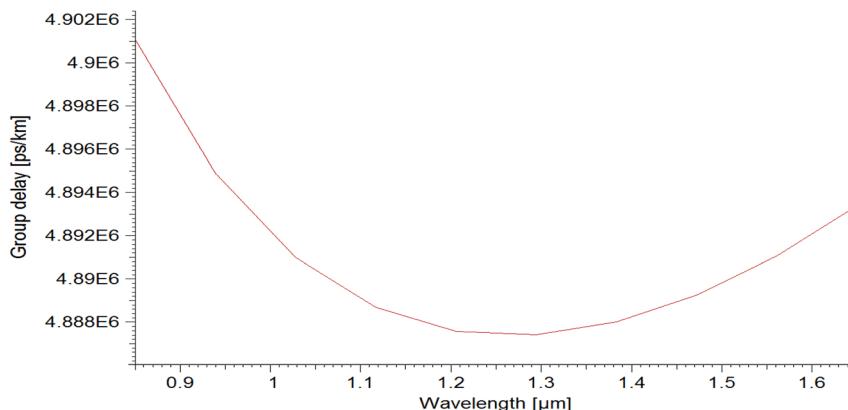
### 3 Results and discussions

We have simulated the designed multi-layer fibre by using optifibre simulation software. The model/group RI are analyzed and sketched with fibre wavelength variations. All the fibre losses and fibre dispersion are simulated and clarified in more details. All the fibre linear polarization (LP) modes and the theoretical fibre cutoff values for the different modes based the designed fibre profile model are detected and clarified by using the finite difference method.

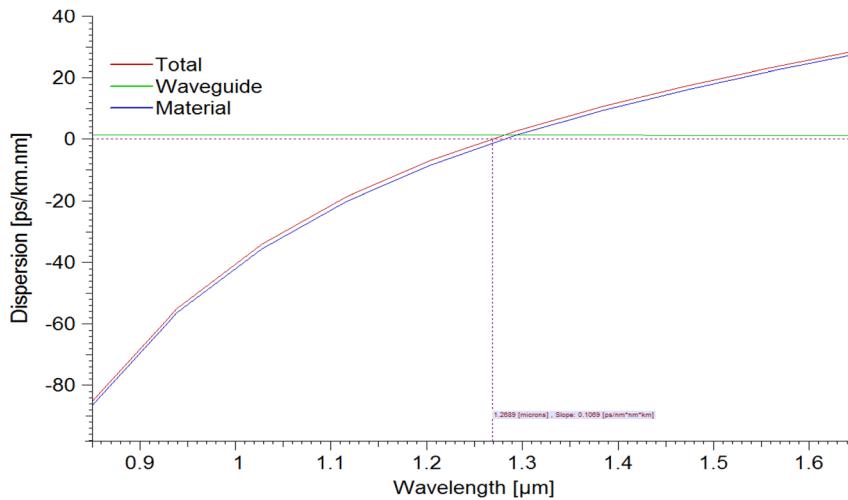
Figure 2 demonstrates the group/model indices variations with the variations of the fibre wavelength. The modal index decreases exponentially through the fibre wavelength of 0.85–1.2 μm and increases exponentially through the fibre wavelength of 1.21–1.65 μm. But the group index decreases linearly through the fibre wavelength of 0.85–1.65 μm. Figure 3 shows the group delay variations in



**Figure 2:** Group/model indices variations with the variations of the fibre wavelength.



**Figure 3:** Group delay variations in relation to the fibre wavelength variations.



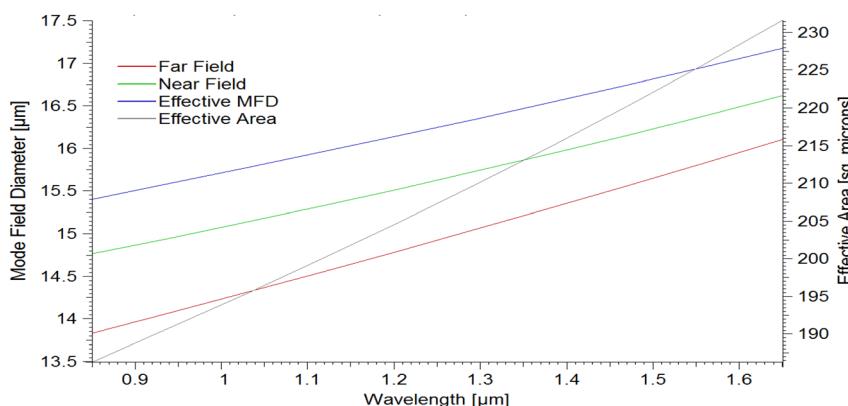
**Figure 4:** The fibre dispersion variations with respect to wavelength.

relation to the fibre wavelength variations. The group delay decreases exponentially through the fibre wavelength of 0.85–1.25  $\mu\text{m}$  and increases exponentially through the fibre wavelength of 1.25–1.65  $\mu\text{m}$ . The min fibre group delay is achieved at 1.25  $\mu\text{m}$  which its value is 4.882  $\mu\text{s}/\text{km}$ .

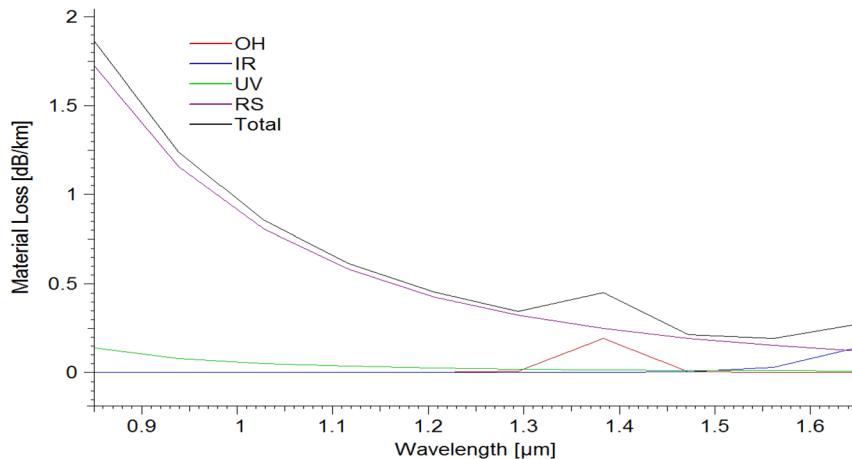
Figure 4 indicates the fibre dispersion variations with fibre wavelength variations. The dispersion is slightly constant at a value of 1  $\text{ps}/\text{nm} \cdot \text{km}$ . The fibre material dispersion

increases exponentially with the fibre wavelength variations. Therefore the resultant total fibre dispersion increases exponentially with the fibre wavelength. The zero dispersion for the designed multi-fibre layers is at 1.2689  $\mu\text{m}$  and the slope of dispersion is 0.1069  $\text{ps}/\text{nm}^2 \cdot \text{km}$  for the designed fibre.

Figure 5 shows the mode field diameter/effective area variations with wavelength. The far and near fibre field



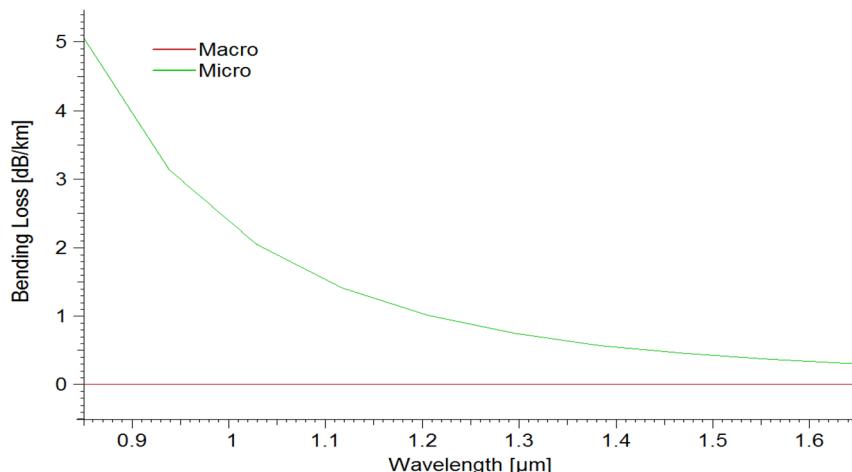
**Figure 5:** The mode field diameter/effective area variations with wavelength.



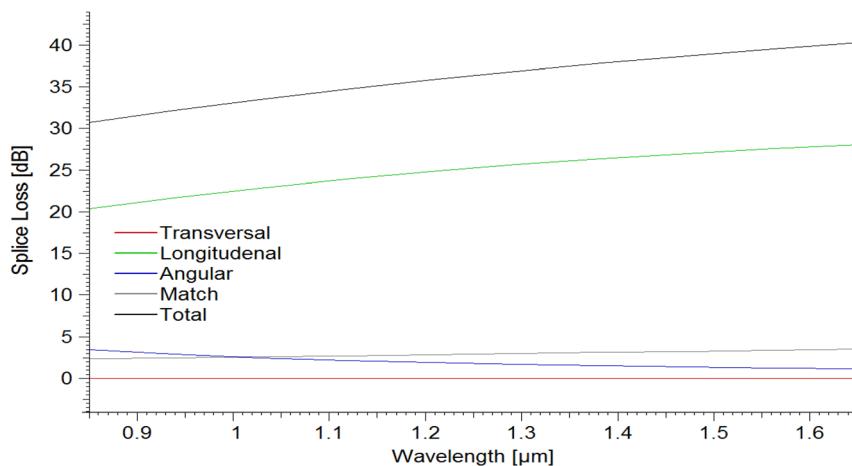
**Figure 6:** Total fibre material losses variations with the fibre wavelength variations.

increases linearly with wavelength. Mode field diameter increases linearly from the value of 15.4–17.2  $\mu\text{m}$  with fibre wavelength variations. Besides the effective fibre area increases linearly with the fibre wavelength variations. The effective fibre area is  $230 \mu\text{m}^2$  at 1.65  $\mu\text{m}$  and the effective fibre area is  $180 \mu\text{m}^2$  at 0.85  $\mu\text{m}$ .

Figure 6 shows the total fibre material losses variations with the fibre wavelength variations. The OH fibre peak loss is 0.25 dB/km at 1.39  $\mu\text{m}$ . The infrared (IR) fibre loss has 0.3 dB/km at 1.65  $\mu\text{m}$ . The ultraviolet (UV) fibre loss decreases linearly to reach 0.01 dB/km at 1.65  $\mu\text{m}$ , while the value of 0.2 dB/km at 0.85  $\mu\text{m}$ . The Rayleigh scattering (RS)



**Figure 7:** Macro/micro fibre bending losses variations versus the fibre wavelength variations.

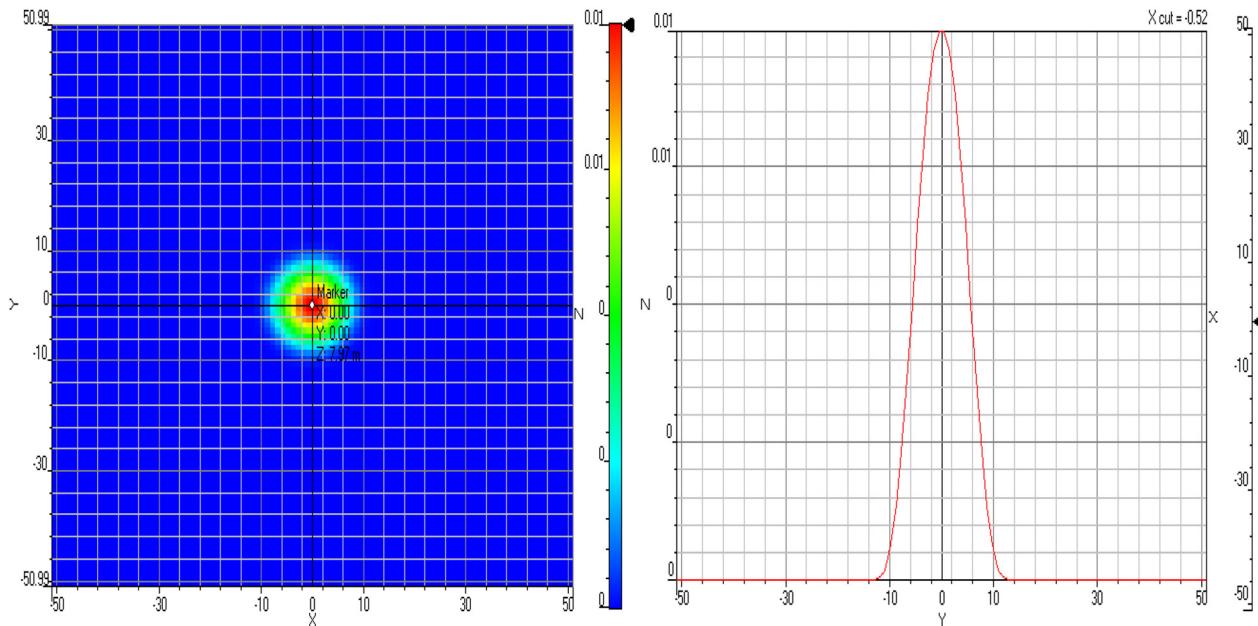


**Figure 8:** Total fibre splice loss variations against the fibre wavelength variations.

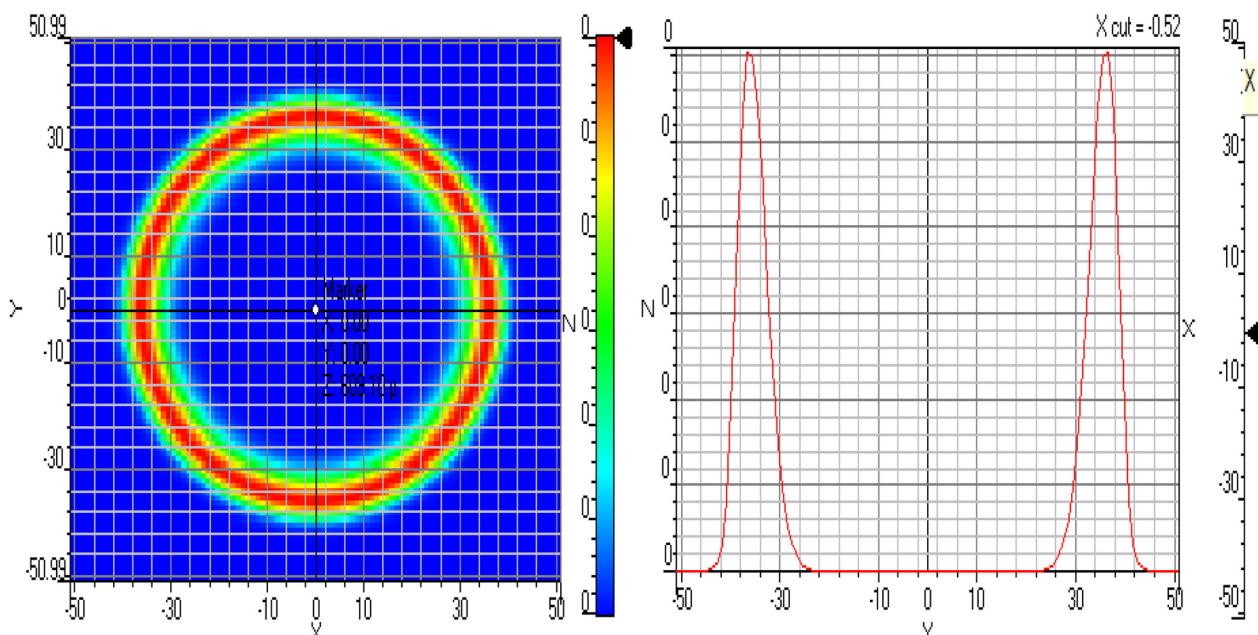
fibre loss decreases exponentially with fibre wavelength variations. Where the max RS fibre loss value is 1.7 dB/km at 0.85  $\mu\text{m}$ , but the min RS fibre loss value is 0.325 dB/km at 1.65  $\mu\text{m}$ . Therefore the resultant total fibre material loss decreases linearly with fibre wavelength variations. Where the total fibre material loss value is 1.852 dB/km at 0.85  $\mu\text{m}$ , but the min total fibre material loss value is 0.3786 dB/km at 1.65  $\mu\text{m}$ .

Figure 7 shows the micro/macro fibre losses of the bending variations versus the fibre wavelength variations. The micro fibre bending loss decreases exponentially from 5 to 0.5 dB/km with the fibre wavelength variations. But the macro fibre bending loss is approximately zero.

Figure 8 demonstrates the total fibre splice loss variations against the fibre wavelength variations. The transversal splice loss is approximately zero, the longitudinal



**Figure 9:** Dominant mode field (DMF) distribution for LP (0, 1) 1.4493825.

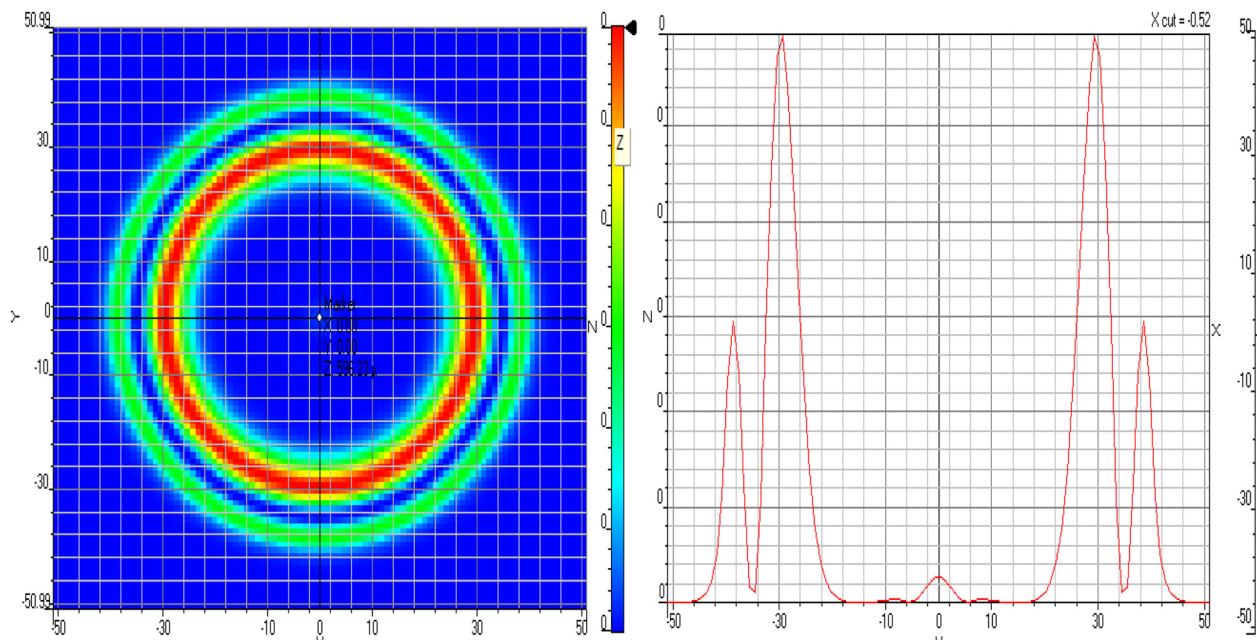


**Figure 10:** DMF distribution for LP (0, 2) 1.4485248.

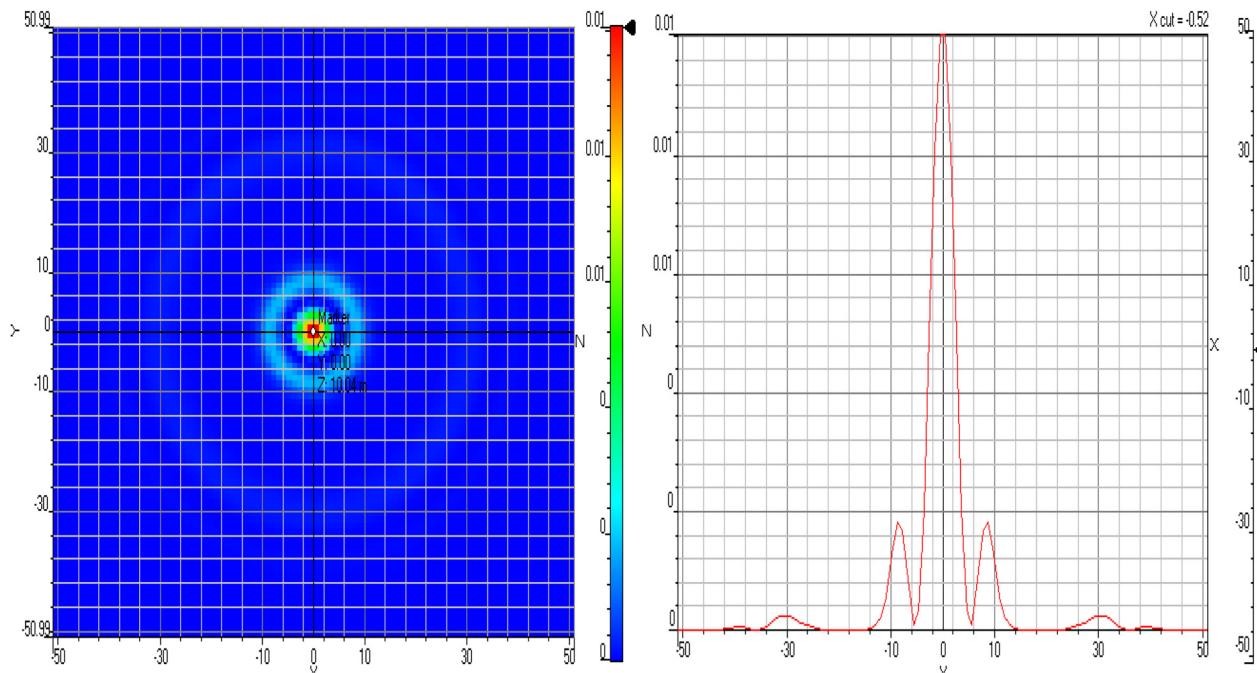
splice loss increases slightly in linear relation from 20 to 25 dB with the fibre wavelength variations from 0.85 to 1.65  $\mu\text{m}$ . Where the angular splice loss decreases linearly from 3 to 0.5 dB. But the match splice loss increases linearly from 2.5 to 5 dB with the fibre wavelength variations. The total fibre splice loss increases linearly from 30 to 40 dB.

The set of Figures 9–13 clarify the dominant mode field distribution for LP (0, 1)  $\rightarrow$  1.4493825, LP (0, 2)  $\rightarrow$  1.4485248,

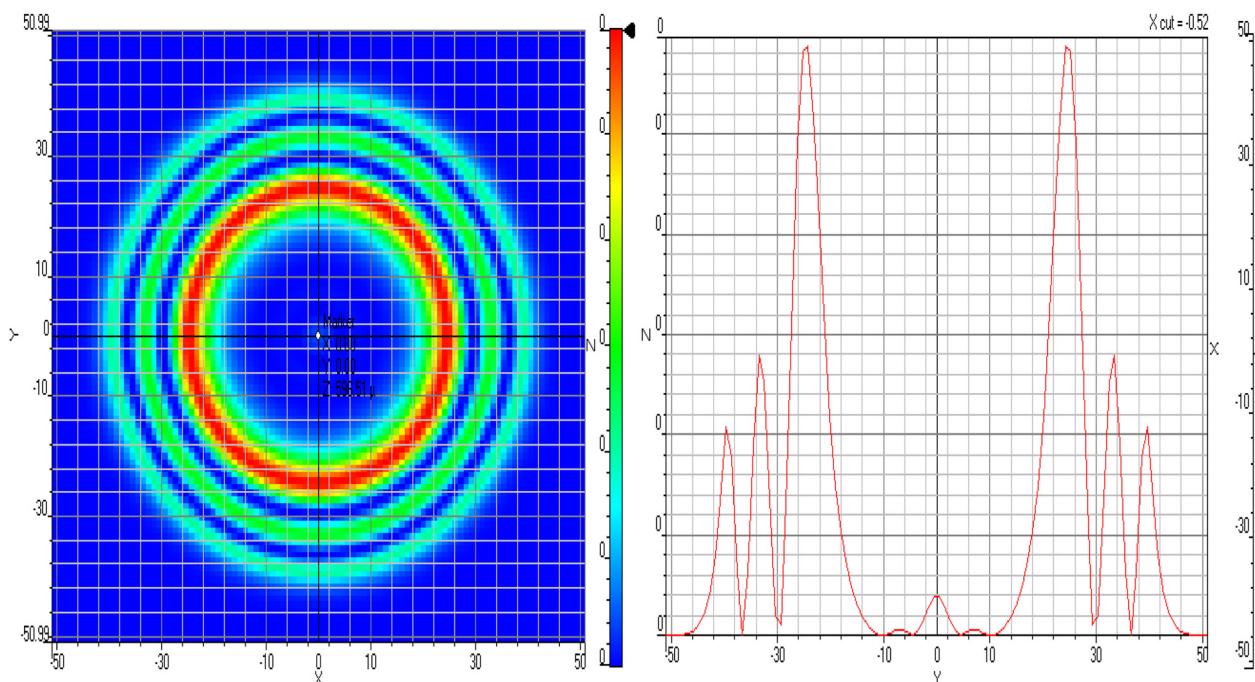
LP (0, 3)  $\rightarrow$  1.4469608, LP (0, 4)  $\rightarrow$  1.4468666 and LP (0, 5)  $\rightarrow$  1.4455431. The mode field distribution is assured in all figures in  $x$ ,  $y$ ,  $z$  directions respectively. Where the other modes for designed multi-layer fibre are LP (1, 1)  $\rightarrow$  1.4485126, LP (1, 2)  $\rightarrow$  1.4484474, LP (1, 3)  $\rightarrow$  1.4469447, LP (1, 4)  $\rightarrow$  1.4455295, LP (1, 5)  $\rightarrow$  1.4452064. While the fibre ITU-T values for the different modes based the designed multi-layer fibre is LP (1, 1)  $\rightarrow$  5.9500000.



**Figure 11:** DMF distribution for LP (0, 3) 1.4469608.



**Figure 12:** DMF distribution for LP (0, 4) 1.4468666.



**Figure 13:** DMF distribution for LP (0, 5) 1.4455431.

## 4 Conclusions

The designed multi-layer fibre is simulated by using opti-fibre simulation software. The model/group RI is demonstrated with fibre wavelength variations. All the fibre losses and fibre dispersion are simulated and clarified in more details. All the fibre linear polarization (LP) modes and the theoretical fibre cutoff values for the different modes based the designed fibre profile model are detected and clarified by using the finite difference method. The study assured that the zero dispersion for the designed multi fibre layer is at  $1.2689 \mu\text{m}$  and the slope of dispersion is  $0.1069 \text{ ps/nm}^2 \text{ km}$  for the designed fibre. More attempts and new research work are performed to reduce the fibre propagation problems.

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**Conflict of interest statement:** The authors declare no conflicts of interest regarding this article.

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